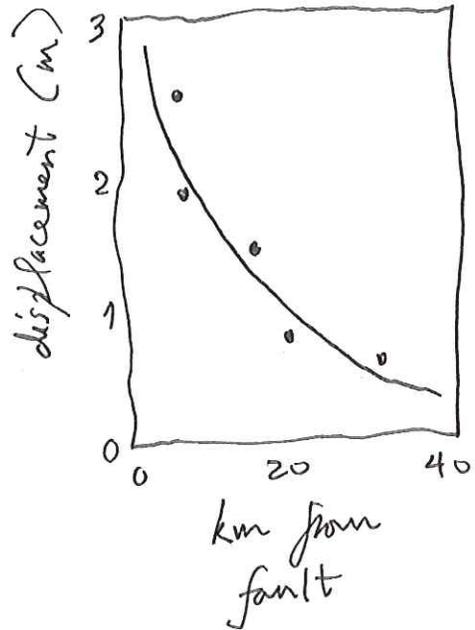
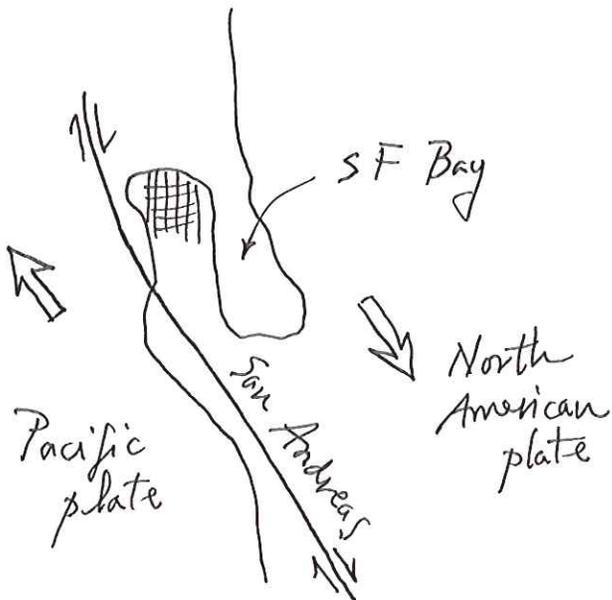
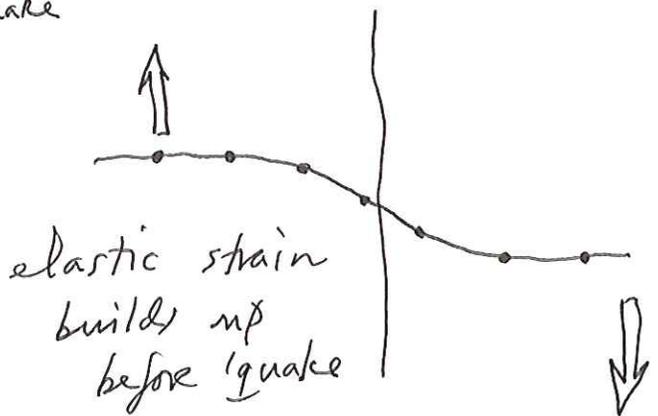
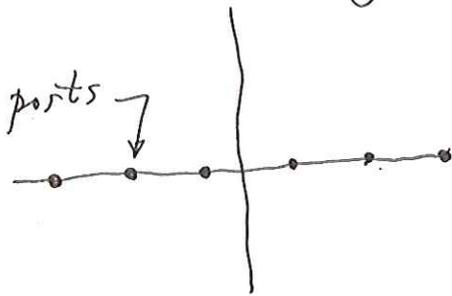


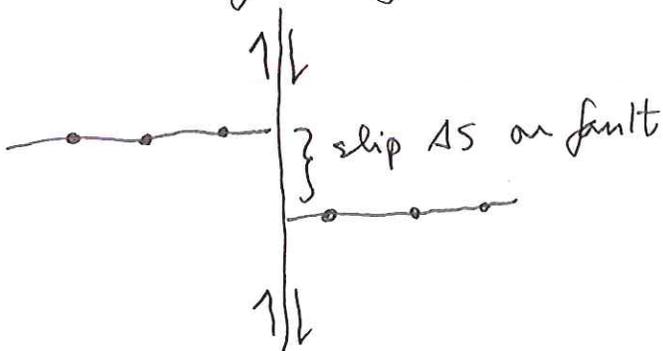
1906 San Francisco earthquake
 H.F. Reid — elastic rebound hypothesis



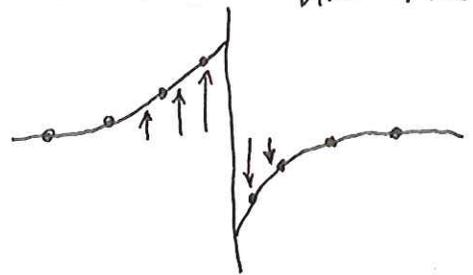
Imaginary fence across
 San Andreas long before quake



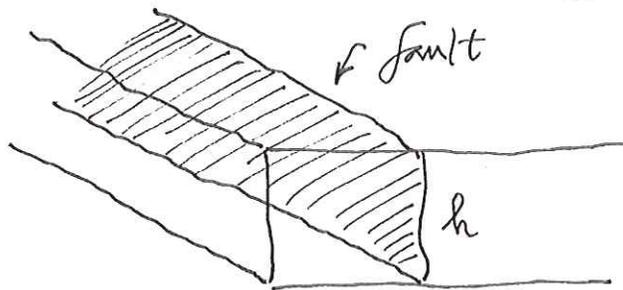
Catastrophic failure when
 the strength of the fault is exceeded



A fence straight just
 before quake would look
 like this

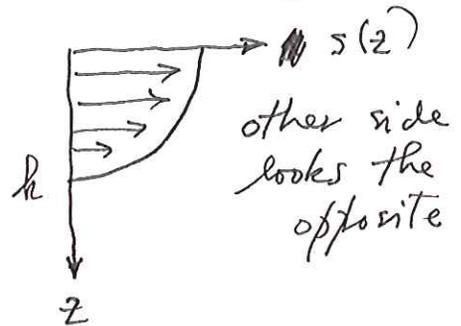


Mathematical model — the quake relieves the stress by an ~~amount~~ amount $\Delta\sigma$ down to a depth h on an infinitely long fault



The slip of each side (as a function of depth z)

$$s(z) = \frac{\Delta\sigma}{\mu} \sqrt{h^2 - z^2}$$



The total slip on the Φ 's surface ($z=0$) is

$$\Delta S = 2 \left(\frac{\Delta\sigma}{\mu} \right) h$$

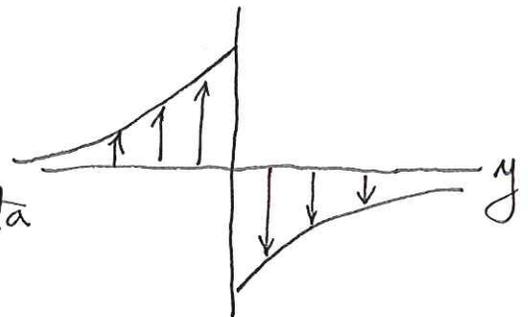
As a function of distance x away from the fault, on the surface of the Φ , the slip is

$$s(y) = \frac{\Delta\sigma}{\mu} \left[\sqrt{h^2 + y^2} - y \right]$$

A fit to Reid's SF quake data gives

$$\Delta S = 5 \text{ m}$$

$h \approx 6 \text{ km}$ — depth of strike-slip faulting



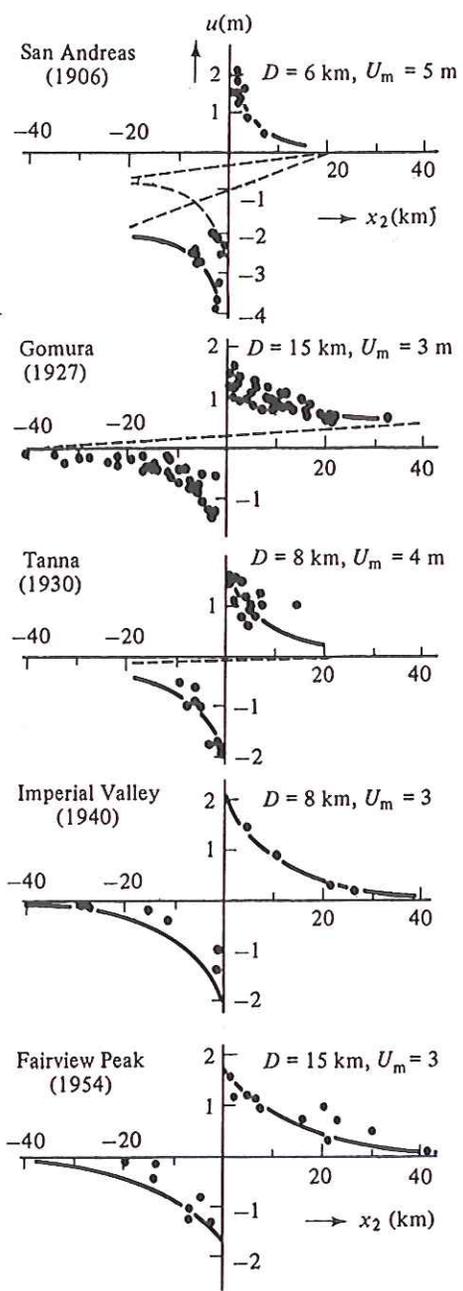


Fig. 4.9. Surface displacements (parallel to the fault strike) associated with several representative strike-slip faults for comparison with the predictions of the vertical strike-slip model (fig. 4.7). Broken lines show corrections for the hypothetical strain accumulation during the period between pre- and post-earthquake surveys. (After Kasahara, 1960.)

$$1 \text{ Nm} = 10^7 \text{ dyne cm}$$

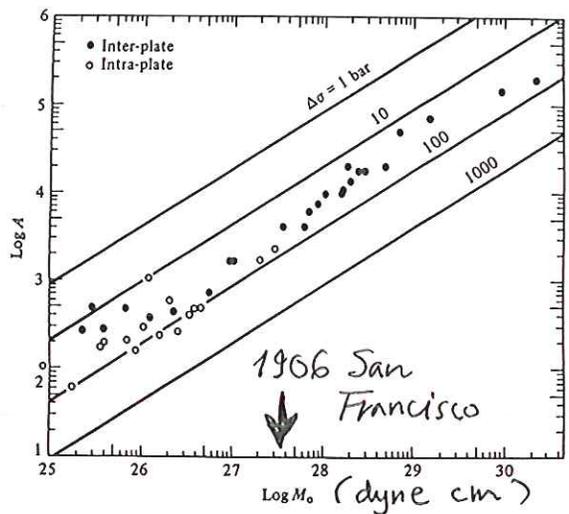


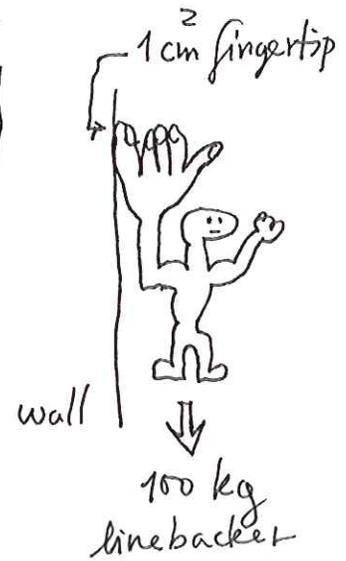
FIGURE 9.25 Area versus moment for inter- and intraplate earthquakes. Note that the interplate earthquakes show little scatter about a stress drop of 30 bars. The intraplate earthquakes have stress drops of ~ 100 bars. (Modified from Kanamori and Anderson, 1975.)

Stress drop:

$$\Delta\sigma = \frac{\mu \Delta s}{2L} = \frac{\overset{\text{crustal rigidity } \mu}{3 \cdot 10^{10} \text{ Pa}} \times 5 \text{ m}}{2 \cdot 6 \cdot 10^3 \text{ m}}$$

$$\Delta\sigma \approx 10 \text{ MPa} = 100 \text{ bars}$$

↑ shear strength
of San Andreas fault

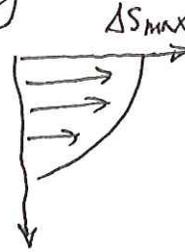


Earthquake moment:

Best measure of the size of an earthquake

$$M_0 = \mu A \bar{\Delta s}$$

↗ fault area
 ↘ average slip



$$\bar{\Delta s} = \frac{\pi}{4} \Delta s_{\max}$$

$$M_0 = (3 \cdot 10^{10}) (6 \cdot 500) \cdot 10^6 \cdot \frac{\pi}{4} \cdot 5 = 4 \cdot 10^{20} \text{ Nm}$$

↑
 500 km
 length of
 rupture

1906 SF quake

Radiated elastic energy

$$E = \frac{1}{2} \Delta\sigma A \bar{\Delta s} = 6 \cdot 10^{16} \text{ Joules (1906 SF quake)}$$

For comparison:

daily US electrical energy consumption: $11 \cdot 10^{16} \text{ J}$

Hiroshima nuclear explosion: $14 \text{ kt} = 6 \cdot 10^{13} \text{ J}$

Mt. Pinatubo eruption: 10^{20} J

same units (1 J = 1 Nm)

$$E = \left(\frac{\Delta\sigma}{2\mu} \right) M_0$$

Typical quake stress drops are in range
 $\Delta\sigma = 1-10$ MPa (say average 3 MPa)

Then

$$E \approx \frac{M_0}{2 \cdot 10^4}$$

Circular fault patch model:



stress drop $\Delta\sigma$ on a circular patch of radius a

$$M_0 = \mu A \Delta\sigma = \frac{16}{7} \Delta\sigma a^3$$

$$= \frac{16}{7\sqrt{\pi^3}} \Delta\sigma A^{3/2}$$

$$M_0 = 0.4 \Delta\sigma A^{3/2}$$

Bigger patches have bigger slip

or on a log-log plot:

$$\log M_0 = \underbrace{\log(0.4 \Delta\sigma)}_{\approx \text{constant}} + \frac{3}{2} \log A$$

↑
slope 3/2

Earthquake magnitude

An older empirical measure of earthquake size. For large earthquakes, now defined in terms of moment \bar{M}_0 by

$$M = \frac{2}{3} \log_{10} \bar{M}_0 - 6.1 \quad \text{--- so-called moment magnitude}$$

1906 SF quake : $M = 7.7$

Combining * and ** gives energy-magnitude relation:

$$\log_{10} E (\text{Joules}) = 1.5 M + 4.8$$

magnitude M	moment \bar{M}_0 (Nm)	energy E (J)
6	$1 \cdot 10^{18}$	$6.3 \cdot 10^{13}$
7	$4 \cdot 10^{19}$	$2 \cdot 10^{15}$
8	$1 \cdot 10^{21}$	$6.3 \cdot 10^{16}$
9	$4 \cdot 10^{22}$	$2 \cdot 10^{18}$

An increase in magnitude $\Delta M = 1$: $10^{1.5} = \underline{\underline{31.6 \text{ times}}}$
as energetic

An increase by $\Delta M = 2$: $10^3 = \underline{\underline{1000 \text{ times}}}$
as energetic

Earthquake statistics:

Gutenberg - Richter frequency-magnitude law

N = number of quakes of magnitude $\geq M$
(in a given region and a given time interval)

$$\log_{10} N = a - bM \quad b \approx 1$$

a decrease by $\Delta M = 1 \Rightarrow$
10 times as many quakes

The constant a depends on size of region and time interval

Corresponding moment-frequency law

$$\log_{10} N = a - b \left(\frac{2}{3} \log_{10} M_0 - 6.1 \right)$$

or with $b = 1$

$$\log_{10} N + \frac{2}{3} \log_{10} M_0 = a + 6.1$$

$$N M_0^{2/3} = 10^{a+6.1}$$

$$N = \underbrace{10^{a+6.1}}_{\text{const}} M_0^{-2/3}$$

-2/3 slope on a log-log plot

M_0 in $N M_0$

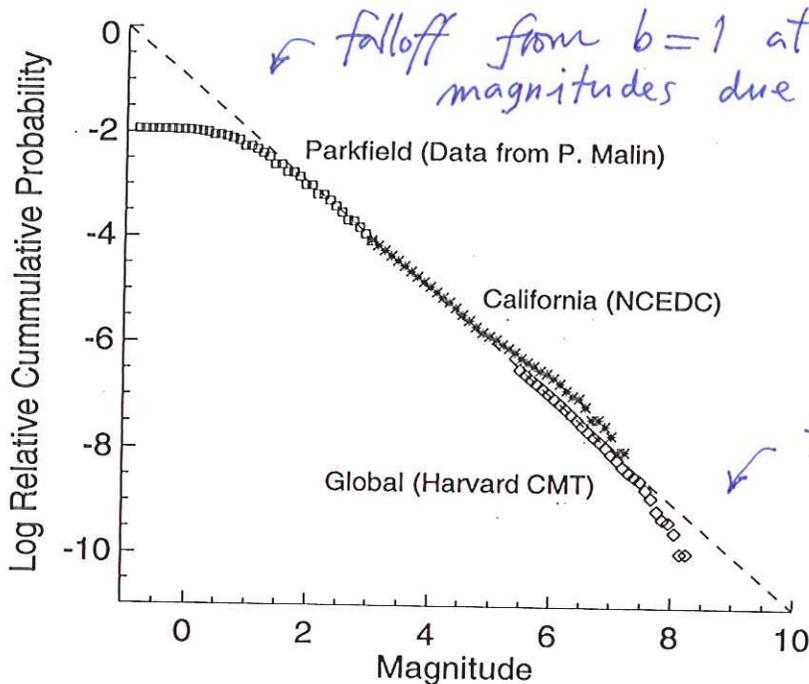
Shallow quakes worldwide:

M	M_0 (Nm)	N (# per year)
9	$4 \cdot 10^{22}$	0.16
8	$1 \cdot 10^{21}$	1.6
7	$4 \cdot 10^{19}$	16
6	$1 \cdot 10^{18}$	160
5	$4 \cdot 10^{16}$	1600
4	$1 \cdot 10^{15}$	16,000

$$\log_{10} N = 8.2 - M$$

$$N = 2 \cdot 10^{14} M_0^{-2/3}$$

about 40 quakes/day worldwide $M \geq 4$.



Total energy released by earthquakes per year

note: this now the interval number rather than the cumulative number

M	$N (M+1 \leq \text{magnitude} \leq M)$	E (Joules/yr)
8	1.4	10^{17}
7	14	$3 \cdot 10^{16}$
6	140	10^{16}
5	1400	$3 \cdot 10^{15}$
4	14,000	10^{15}

Earthquake energy release is dominated by the occasional large earthquake

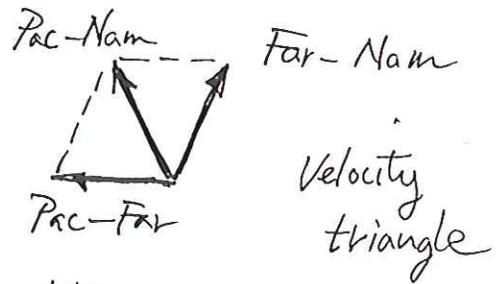
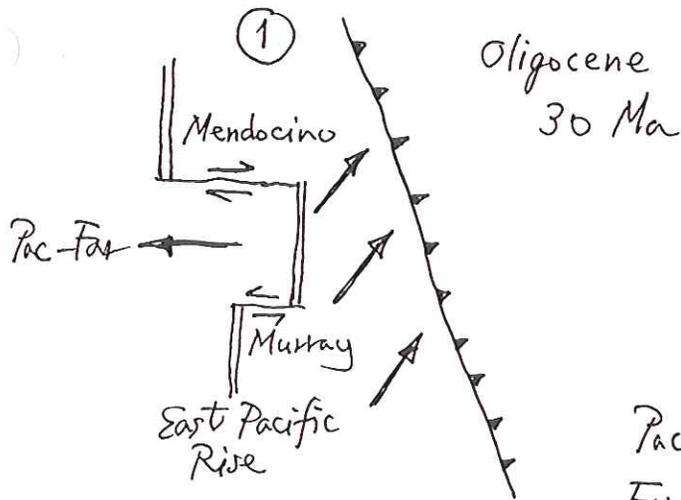
total $\approx 2 \cdot 10^{17}$ J/yr

or $6 \cdot 10^9$ W

$\approx \frac{1}{5000}$ x total heat flow

This a measure of the thermal efficiency of the \oplus as a heat engine.

Evolution of the California Margin



Pac: Pacific plate
Far: Farallon plate
Nam: North American plate

