

Summarizing Eulerian conservation laws

$$1. \text{ mass (continuity) : } \frac{\partial}{\partial t} \rho + \nabla \cdot (\rho \underline{u}) = 0 \quad \text{or} \\ \frac{D}{Dt} \rho + \rho \nabla \cdot \underline{u} = 0$$

$$2. \text{ momentum : } \rho \frac{D}{Dt} \underline{u} = \nabla \cdot \underline{T} + \underline{f}$$

$$3. \text{ angular momentum : } \underline{T}^T = \underline{T}$$

$$4. \text{ internal energy : } \rho \frac{D}{Dt} \varepsilon + \nabla \cdot \underline{H} = \dot{h} + \underline{T} : \underline{\varepsilon}$$

$$5. \text{ Clausius-Duhem : } \rho \frac{D}{Dt} \eta \geq \frac{\dot{h}}{\theta} - \nabla \cdot \left(\frac{\underline{H}}{\theta} \right)$$

We've also obtained the Lagrangian form of the mass conservation law.

Let $\underline{r}(\underline{x}, t)$ be the Lagrangian description of the motion.

Comoving volume $V(t)$:

$$M(t) = \int_{V(t)} \rho_E(\underline{r}, t) dV = \int_{V(0)} \rho_L(\underline{x}, t) J(\underline{x}, t) dV_0$$

where $J(\underline{x}, t) = \det \begin{vmatrix} \partial r_1 / \partial x_1 & \partial r_1 / \partial x_2 \\ \text{etc.} \end{vmatrix}$

$$= M(t) = \int_{V(t)} \rho_L(\underline{x}, t) dV_0$$

$$\rho_L(\underline{x}, t) J(\underline{x}, t) = \rho_L(\underline{x}, 0) \equiv \rho_0(\underline{x})$$

↑
initial density
of particle \underline{x}

To obtain the Lagrangian version of the momentum law we rewrite the Eulerian form slightly

$$\text{let } \underline{f}_E(\underline{r}, t) = \rho_E(\underline{r}, t) \underline{g}_E(\underline{r}, t)$$

↑
body force per unit mass.

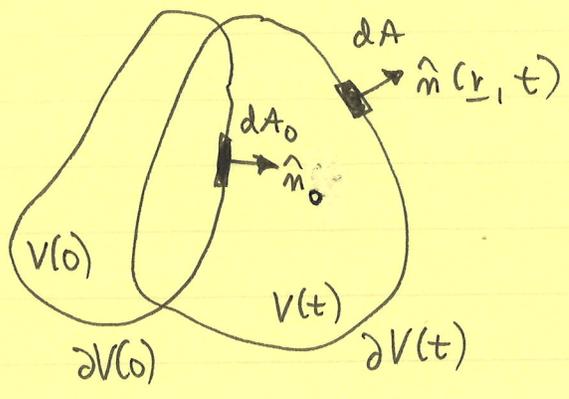
$$\rho_E \underline{D}_t \underline{u}_E = \nabla \cdot \underline{T}_E + \rho_E \underline{g}_E$$

$$\underline{T}_E(\underline{r}, t) = \underline{T}_E^T(\underline{r}, t) \text{ is called the } \underline{\text{Cauchy stress}}$$

Regarded as a linear operator :

$$\underbrace{d\underline{F}(\underline{r}, t)}_{\text{force acting on deformed area element}} = \underbrace{\hat{n}(\underline{r}, t) dA}_{\text{deformed area element}} \cdot \underline{T}(\underline{r}, t)$$

Define first Piola-Kirchoff stress tensor by



Note: we do not define $\underline{T}_L(x, t) = \underline{T}_E(r(x, t), t)$ "as usual"

~~$dF = \hat{n}(r, t) dA \cdot \underline{T}(r, t)$~~
 ~~$dF = \hat{n}_0 dA_0 \cdot \underline{T}_L(x, t)$~~

$$dF = \hat{n} dA \cdot \underline{T} = \hat{n}_0 dA_0 \cdot \underline{T}_L, \quad \text{or written out}$$

~~$\hat{n}(r(x, t), t) \cdot \underline{T}(r(x, t), t)$~~

$$\begin{aligned} \hat{n}(r(x, t), t) dA(r(x, t), t) \cdot \underline{T}_E(r(x, t), t) \\ = \hat{n}_0(x) dA_0(x) \cdot \underline{T}_L(x, t) \end{aligned}$$

Viewed as a linear operator, \underline{T}_L gives the incremental surface force acting across the deformed surface element in terms of the initial $\hat{n}_0 dA_0$ of that element.

$$\underbrace{dF \text{ (on } \hat{n} dA)}_{\text{result is force on deformed element}} = \underbrace{\hat{n}_0 dA_0}_{\text{initial element goes in slot}} \cdot \underline{T}_L$$

For this reason, Malvern refers to $\underline{\underline{T}}$ as a "two-point" tensor.

$$\text{Go back to } \rho_E \underline{D}_t \underline{u}_E = \nabla \cdot \underline{\underline{T}}_E + \rho_E \underline{g}_E$$

Integrate over a comoving volume $V(t)$:

$$\begin{aligned} \int_{V(t)} \rho_E \underline{D}_t \underline{u}_E \, dV &= \int_{V(t)} \nabla \cdot \underline{\underline{T}}_E \, dV + \int_{V(t)} \rho_E \underline{g}_E \, dV \\ &= \int_{\partial V(t)} \hat{n}(\underline{r}, t) \cdot \underline{\underline{T}}_E(\underline{r}, t) \, dA \\ &\quad + \int_{V(t)} \rho_E \underline{g}_E \, dV \end{aligned}$$

Transform variable of integration from \underline{r} to \underline{x} .
Domain $V(t) \rightarrow V_0$.

$$\begin{aligned} \int_{V(t)} \rho_E \underline{D}_t \underline{u}_E \, dV &= \int_{V_0} \rho_E \underline{D}_t \underline{u}_L \, J \, dV_0 \\ &= \int_{V_0} \rho_0 \underline{D}_t \underline{u}_L \, dV_0 = \int_{V_0} \rho_0 \underline{D}_t^2 \underline{r}(\underline{x}, t) \, dV_0 \end{aligned}$$

$$\text{Likewise : } \int_{V(t)} \rho_E \underline{g}_E \, dV = \int_{V_0} \rho_0 \underline{g}_L(\underline{x}, t) \, dV_0$$

(This is why we use \underline{g} instead of \underline{f})

Finally:
$$\int_{\partial V(t)} \hat{n} \cdot \underline{T}_E dA = \int_{\partial V(t)} \hat{n}_0 \cdot \underline{T}_L dA_0$$

$$= \int_{V(t)} \underline{\rho}_x \cdot \underline{T}_L(\underline{x}, t) dV$$

(This is why the PK stress is defined as it is)

Now $V(t)$ is arbitrary, so:

$$\rho_0(\underline{x}) D_t^2 \underline{r}(\underline{x}, t) = \underline{\rho}_x \cdot \underline{T}_L(\underline{x}, t) + \rho_0(\underline{x}) \underline{g}_L(\underline{x}, t)$$

Note appearance of $\rho_0(\underline{x})$, not $\rho_L(\underline{x}, t)$.

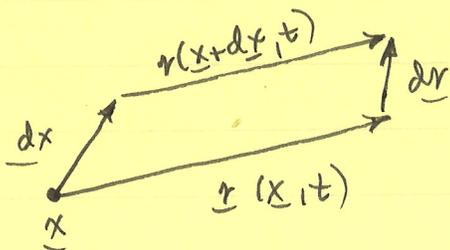
Note D_t^2 is not nonlinear \sim in $\rho_0 D_t \underline{u}$

How is $\underline{T}_L(\underline{x}, t)$ related to $\underline{T}_E(\underline{r}, t)$?

We must find out how $\hat{n} dA$ is related to $\hat{n}_0 dA_0$. This is a purely kinematic question.

Given Lagrangian description $\underline{r}(\underline{x}, t)$.

Consider a small ball of material around \underline{x} at $t=0$.



How is $d\underline{r}$ related to $d\underline{x}$?

$$\begin{aligned} d\underline{r} &= \underline{r}(\underline{x} + d\underline{x}, t) - \underline{r}(\underline{x}, t) \\ &= \underline{r}(\underline{x}, t) + d\underline{x} \cdot \underline{\rho}_x \underline{r}(\underline{x}, t) + \dots - \underline{r}(\underline{x}, t) \end{aligned}$$

~~$\underline{dr} = \underline{dx} \cdot \nabla_{\underline{x}} \underline{r}(\underline{x}, t)$~~ $\underline{dr} = \underline{dx} \cdot \nabla_{\underline{x}} \underline{r}(\underline{x}, t)$

Customary to define deformation gradient $\underline{\underline{F}}(\underline{x}, t)$ by

$$\underline{\underline{F}}^T(\underline{x}, t) = \nabla_{\underline{x}} \underline{r}(\underline{x}, t) \text{ so that}$$

$$\underline{dr} = \underline{\underline{F}} \cdot \underline{dx} = \underline{dx} \cdot \underline{\underline{F}}^T$$

$\underline{\underline{F}}(\underline{x}, t)$ is the linear operator that gives \underline{dr} in terms of \underline{dx}

Note that $J(\underline{x}, t) = \det \underline{\underline{F}}(\underline{x}, t)$

By definition $\underline{r}(\underline{x}, 0) = \underline{x}$ $\underline{\underline{F}}(\underline{x}, 0) = \underline{\underline{I}}$, $J(\underline{x}, 0) = 1$
 If the deformation is continuous, then $J(\underline{x}, t) > 0$ for all t .

$\nabla \underline{r}(\underline{x}, t)$ exists

As a result $\underline{\underline{F}}$ is always invertible.

The inverse of a tensor $\underline{\underline{F}}$ (if it \exists) is defined by

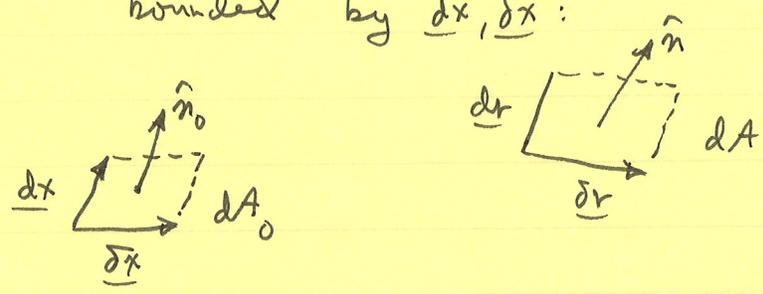
$$\underline{u} = \underline{\underline{F}} \cdot \underline{v} \iff \underline{v} = \underline{\underline{F}}^{-1} \cdot \underline{u}$$

In this case $\underline{dx} = \underline{\underline{F}}^{-1} \cdot \underline{dr} = \underline{dr} \cdot \underline{\underline{F}}^{-T}$

$$\underline{\underline{F}}^{-T}(\underline{r}, t) = \nabla_{\underline{r}} \underline{x}(\underline{r}, t)$$

Now to relate $\hat{n} dA$ to $\hat{n}_0 dA_0$.

Let the initial dA_0 be a parallelogram bounded by $\underline{dx}, \underline{\delta x}$:



Then $\hat{n}_0 dA_0 = \underline{dx} \times \underline{\delta x}$

$\hat{n} dA = \underline{dr} \times \underline{\delta r}$

i.e. $n_{0i} dA_0 = \epsilon_{ijk} dx_j \delta x_k$

$n_i dA = \epsilon_{ijk} dr_j \delta r_k$ [$n_r dA = \epsilon_{rpg} dr_r \delta r_g$]

But $dx_j = F_{jP}^{-1} dr_P$

~~delta x_k~~ $\delta x_k = F_{kq}^{-1} \delta r_q$

So $n_{0i} dA_0 = \epsilon_{ijk} F_{jP}^{-1} F_{kq}^{-1} dr_P \delta r_q$

Multiply both sides by ~~delta~~ F_{ir}^{-1} :

$F_{ir}^{-1} n_{0i} dA_0 = \epsilon_{ijk} F_{ir}^{-1} F_{jP}^{-1} F_{kq}^{-1} dr_P \delta r_q$

We use a general formula for the determinant:

$$\epsilon_{rpg} (\det M) = \epsilon_{ijk} M_{ir} M_{jp} M_{kg}$$

$$\epsilon_{rpg} (\det F^{-1}) = \epsilon_{ijk} \cancel{J^{-1}} J^{-1} = \epsilon_{ijk} F_{ir}^{-1} F_{jp}^{-1} F_{kg}^{-1}$$

$$F_{ir}^{-1} n_{oi} dA_o = J^{-1} \epsilon_{rpg} dr_p dr_g \\ = J^{-1} n_r dA$$

$$n_r dA = J n_{oi} dA_o F_{ir}^{-1} \quad \text{or}$$

$$\hat{n} dA = J \hat{n}_o \cdot \underline{F}^{-1} dA_o$$

$$\hat{n} \cdot \underline{T}_E dA = J \hat{n}_o \cdot \underline{F}^{-1} \cdot \underline{T}_E dA_o = \hat{n}_o \cdot \underline{T}_L dA_o$$

$$\underline{T}_L = J \underline{F}^{-1} \cdot \underline{T}_E$$

$$\underline{T}_L(\underline{x}, t) = J(\underline{x}, t) \underline{F}^{-1}(\underline{r}(\underline{x}, t), t) \cdot \underline{T}_E(\underline{r}(\underline{x}, t), t)$$

rather than $\underline{T}_L(\underline{x}, t) = \underline{T}_E(\underline{r}(\underline{x}, t), t)$

The inverse relationship is

$$\underline{T}_E = J^{-1} \underline{F} \cdot \underline{T}_L$$

Note that $\underline{T}_L^T = J \underline{T}_E^T \underline{F}^{-T} = J \underline{T}_E \underline{F}^{-T}$

$$\underline{T}_L^T \neq \underline{T}_L$$

The (first) Piola-Kirchhoff stress tensor is not symmetric even though \underline{T}_E is.

$$\underline{T}_L^T = \underline{F} \cdot \underline{T}_L \cdot \underline{F}^{-T} \text{ can be regarded as ang. mom. cons. law}$$

Now consider the conservation of energy law

$$\rho_E D_t \underline{w}_E + \nabla \cdot \underline{H}_E = h_E + \underline{T}_E : \underline{\underline{\epsilon}}$$

Write $h_E = \rho_E \alpha_E$ $\alpha_E(r, t) = \text{rate of external heating / unit mass}$

Integrate over $V(t)$ as before.

Define $\underline{H}_L(\underline{x}, t)$ by

$$\hat{n} dA \cdot \underline{H}_E = \hat{n}_0 dA_0 \cdot \underline{H}_L$$

$$\underline{H}_L = J \underline{F}^{-1} \cdot \underline{H}_E$$

$$\underline{H}_E = J^{-1} \underline{F} \cdot \underline{H}_L$$

Viewed as a linear functional $\underline{H}_L(\underline{x}, t)$ gives the heat flux through a deformed patch in terms of the corresponding undeformed patch $\hat{n}_0 dA_0$.

$$\int_{r(t)} [\rho_0 D_t u_L - \nabla_x \cdot \underline{H}_L - \rho_0 \alpha_L] dV_0 = \int_{r(t)} \underline{T}^E : \underline{\underline{\epsilon}} dV$$

need to transform this.

Considers $D_t \underline{F}^T = D_t \nabla_x r(\underline{x}, t) = \nabla_x D_t r(\underline{x}, t)$

$$= \nabla_x u_E(r(\underline{x}, t), t)$$

$$= \nabla_x r(\underline{x}, t) \cdot \nabla_x u_E(r(\underline{x}, t), t)$$

$$= \nabla_x u_E(r(\underline{x}, t), t) \cdot \underline{F}(\underline{x}, t)$$

$\nabla_x u_E(r(\underline{x}, t), t) = D_t \underline{F}^T(\underline{x}, t) \cdot \underline{F}^{-1}(\underline{x}, t)$

$$D_t \underline{F}^T(\underline{x}, t) = \nabla_x u_E(r(\underline{x}, t), t) \cdot \underline{F}(\underline{x}, t)$$

$$\underline{T}^E : \underline{\underline{\epsilon}} = T_{ij}^E \partial_j u_i = T_{ij}^E (D_t F_{jk}^T) F_{ki}^{-1}$$

$$\int_{r(t)} \underline{T}^E : \underline{\underline{\epsilon}} dV = \int_{r(t)} J F_{ki}^{-1} T_{ij}^E D_t F_{jk}^T dV_0$$

$$= \int_{r(t)} T_{kj}^L D_t F_{jk} dV_0$$

$$= \int_{r(t)} \underline{T}^L : D_t \underline{F} dV_0 = \int_{r(t)} \underline{T}^L : D_t \underline{F} dV_0$$

$$\rho_0(\underline{x}) D_t \underline{u}_L(\underline{x}, t) + \underline{\nabla}_x \cdot \underline{H}_L(\underline{x}, t) = \rho_0(\underline{x}) \underline{\delta}_L(\underline{x}, t) + \underline{T}_L(\underline{x}, t) \bullet \bullet D_t \underline{F}(\underline{x}, t)$$

By similar reasoning the Lagrangian form of the Clausius - Duhem \neq is :

$$\rho_0(\underline{x}) D_t S_L(\underline{x}, t) \geq - \underline{\nabla}_x \cdot [\underline{\theta}_L^{-1}(\underline{x}, t) \underline{H}_L(\underline{x}, t)] + \rho_0(\underline{x}) \underline{\theta}_L(\underline{x}, t)^{-1} \underline{\delta}_L(\underline{x}, t)$$

Some do not regard $\rho_0 D_t^2 \underline{x} = \underline{\nabla}_x \cdot \underline{T}_L + \rho_0 \underline{g}_L$ as strictly Lagrangian because of the two-point nature of $\underline{T}_L(\underline{x}, t)$

$$\hat{n}_0 dA_0 \cdot \underline{T}_L(\underline{x}, t) = \underline{dF} \text{ is the force on the deformed patch } \hat{n} dA$$

Note that $\hat{n}_0 \cdot \underline{T}_L$ is the force on the deformed patch measured per unit undeformed area.

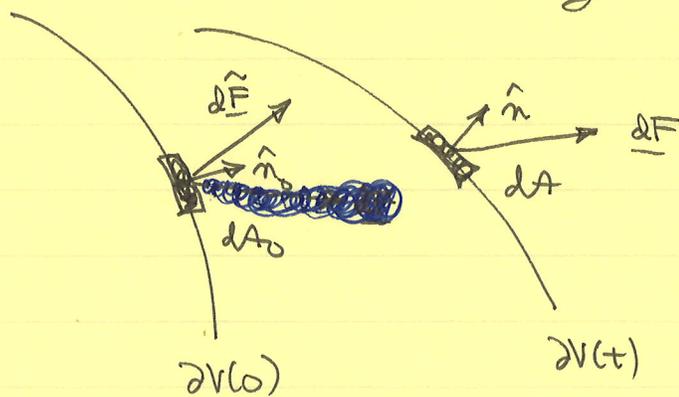
This has led to the introduction of the second Piola Kirchhoff stress tensor, defined by

$$\hat{n}_0 dA_0 \cdot \underline{\underline{\tilde{T}}}_L = d\underline{\underline{\tilde{F}}} = \underline{\underline{F}}^{-1} \cdot d\underline{\underline{F}} = \underline{\underline{F}}^{-1} \cdot (\hat{n} dA \cdot \underline{\underline{T}}_E)$$

The force $d\underline{\underline{\tilde{F}}}$ is related to $d\underline{\underline{F}}$ in the same way that an undeformed ~~vector~~ vector differential $d\underline{x}$ is related to the deformed $d\underline{r}$:

$$d\underline{x} = \underline{\underline{F}}^{-1} \cdot d\underline{r}$$

The picture is (note that \hat{n}_0 is rotated to \hat{n} by same amount $d\underline{\underline{\tilde{F}}}$ is rotated to $d\underline{\underline{F}}$)



$d\underline{\underline{\tilde{F}}}$ is attached to \underline{x} whereas $d\underline{\underline{F}}$ is attached to $\underline{r}(x,t)$

How is $\underline{\underline{\tilde{T}}}_L$ related to $\underline{\underline{T}}_L$?

$$\begin{aligned} \hat{n}_0 dA_0 \cdot \underline{\underline{\tilde{T}}}_L &= \underline{\underline{F}}^{-1} \cdot [J \hat{n}_0 dA_0 \cdot \underline{\underline{F}}^{-1} \cdot \underline{\underline{T}}_E] \\ &= J \hat{n}_0 dA_0 \cdot \underline{\underline{F}}^{-1} \cdot \underline{\underline{T}}_E \cdot \underline{\underline{F}}^{-T} \end{aligned}$$

$$\underline{\tilde{T}}_L = J \underline{F}^{-1} \cdot \underline{T}_E \cdot \underline{F}^{-T}$$

Note that $\underline{\tilde{T}}_L^T = J \underline{F}^{-1} \cdot \underline{T}_E^T \cdot \underline{F}^{-T} = \underline{T}_L$

$$\underline{\tilde{T}}_L \text{ is symmetric}$$

$$\underline{T}_E = J^{-1} \underline{F} \cdot \underline{\tilde{T}}_L \cdot \underline{F}^T$$

also:

$$\underline{\tilde{T}}_L = \underline{F}^{-1} \cdot \underline{T}_E^T$$

Also:

$$\underline{\tilde{T}}_L = \underline{T}_L \cdot \underline{F}^{-T}$$

$$\underline{T}_L = \underline{\tilde{T}}_L \cdot \underline{F}^T$$

Using the latter form we can express the momentum equation in terms of $\underline{\tilde{T}}_L$

also:

$$\underline{T}_L = \underline{F} \cdot \underline{\tilde{T}}_L^T$$

$$\rho_0 \underline{D}_t^2 \underline{x} = \underline{r}_x \cdot [\underline{\tilde{T}}_L \cdot \underline{F}^T] + \rho_0 \underline{g}_L$$

~~also define $\underline{H}_L(\underline{x}, t)$ by $\underline{H}_L = \underline{F}^{-1} \cdot \underline{H}$~~

Malvern page 232 shows that

~~$\underline{H}_L = \underline{F} \cdot \underline{H}$~~

$$\int_{V(t)} \underline{T}_E : \underline{\underline{\epsilon}} \, dV = \int_{V(b)} \underline{\tilde{T}}_L : \underline{D}_t \underline{E} \cdot dV \quad \text{where}$$

$$\underline{\underline{E}}(\underline{x}, t) \equiv \frac{1}{2} [\underline{\underline{F}}^T \cdot \underline{\underline{F}} - \underline{\underline{I}}] \text{ is the (finite) strain tensor}$$

Thus the strictly Lagrangian version of the internal energy equation is:

$$\rho_0 D_t \mathcal{U}_L + \underline{\nabla}_x \cdot \underline{\underline{H}}_L = \rho_0 \mathcal{X}_L + \underline{\underline{T}}_L : D_t \underline{\underline{E}}$$

And, finally, the CD \neq :

$$\rho_0 D_t \mathcal{S}_L \geq - \underline{\nabla}_x \cdot [\theta_L^{-1} \underline{\underline{H}}_L] + \rho_0 \theta_L^{-1} \mathcal{X}_L$$